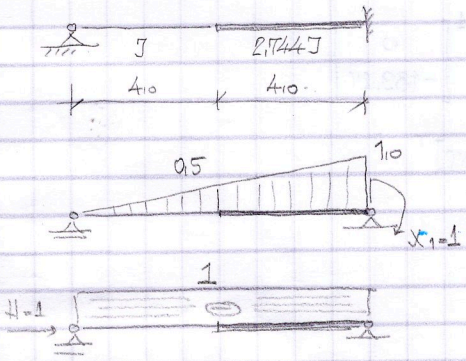


Štapa	i	k	λ	μ
1	1	3	1	0
2	1	2	0,6247	0,78087

$E_b = 3 \cdot 10^7 \text{ kN/m}^2$      $E_c = 21 \cdot 10^7 \text{ kN/m}^2$  ;  $F_c = 48 \text{ cm}^2$   
 $J = \frac{30 \cdot 50^3}{12} = 312500 \text{ cm}^4 = J_b$  ;  $J = \frac{30 \cdot 70^3}{12} = 857500 \text{ cm}^4 = 2,744 J_b$   
 $F = 30 \cdot 50 = 1500 \text{ cm}^2 = F_b$  ;  $F = 30 \cdot 70 = 2100 \text{ cm}^2 = 1,4 F_b$

Matrice krutosti štapova

- Štapa 1



$EJ_c \alpha_{11} = \frac{1}{3} \cdot 0,5^2 \frac{4,00}{1} + \frac{1}{6} [0,5 \cdot (2 \cdot 0,5 + 1,0) + 1,0 \cdot (0,5 + 2 \cdot 1,0)] \cdot \frac{4,00}{2,744} = 1,183673469$   
 $EJ_c \delta = 12 \cdot \frac{4,0}{1} + 12 \cdot \frac{4,0}{1,40} = 6,857142857 \cdot \frac{J_c}{F_c}$   
 $EJ_c \delta = \frac{312500 \cdot 10^{-8}}{1500 \cdot 10^{-4}} = 0,142857142$   
 $\frac{1}{8} = EJ_c \cdot \gamma_{10}$   
 $d_{11} = \frac{1}{\alpha_{11}} = EJ_c \cdot 0,84483$

$K_1 = K_1^* = EJ_c$

1	2	5	6	7	
100	0	-70	0	0	1
0	0,0132	0	-0,0132	0,1056	2
-70	0	70	0	0	5
0	-0,0132	0	0,0132	-0,1056	6
0	0,1056	0	-0,1056	0,84483	7

$EJ_c = 3 \cdot 10^7 \cdot 312500 \cdot 10^{-8} = 93750 \text{ kNm}^2$

- Štapa 2

$K_2 = \frac{E_c F_c}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \frac{21 \cdot 10^7 \cdot 48 \cdot 10^{-4}}{6,403} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$  ;  $T_2 = \begin{bmatrix} 0,6247 & 0,78087 & 0 & 0 \\ 0 & 0 & 0,6247 & 0,78087 \end{bmatrix}$

$K_2^* = T_2^T K_2 T_2 = \begin{bmatrix} 0,6247 & 0 \\ 0,78087 & 0 \\ 0 & 0,6247 \\ 0 & 0,78087 \end{bmatrix} \frac{21 \cdot 48 \cdot 10^3}{6,403} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} 0,6247 & 0,78087 & 0 & 0 \\ 0 & 0 & 0,6247 & 0,78087 \end{bmatrix}$

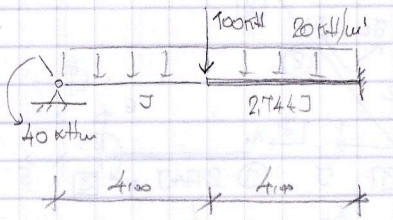
$K_2^* = \frac{21 \cdot 48 \cdot 10^3}{6,403}$

1	2	3	4	
0,3903	0,4878	-0,3903	-0,4878	1
	0,6098	-0,4878	-0,6098	2
		0,3903	0,4878	3
			0,6098	4

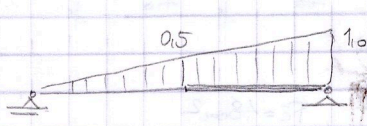
MATRICA KRUTOSTI SISTEMA

$K^* = \begin{bmatrix} 1 & 2 \\ 717693,4484 & 76792,50351 \\ & 97236,0 & 1 \end{bmatrix}$

VEKTOR EKVIVALENTNOS OPT.



$$EJ_c \delta_{10} = \frac{1}{6} \cdot 0.5 \cdot (40 - 2 \cdot 340) \cdot \frac{4.0}{1} - \frac{1}{3} \cdot 0.5 \cdot 40 \cdot \frac{4.0}{1} - \frac{1}{6} \cdot 340 \cdot (0.5 + 2 \cdot 4.0) \cdot \frac{4.0}{2.744} - \frac{1}{3} \cdot (0.5 + 1.0) \cdot 40 \cdot \frac{4.0}{2.744} = -475.6656348$$



$$X_1 = - \frac{EJ_c \delta_{10}}{EJ_c \delta_{11}} = ?$$

$$Q_1 = Q_1^* = \begin{bmatrix} 1 & 2 & 5 & 6 & 7 \\ 0 & -89.27 & 0 & -170.73 & 365.84 \end{bmatrix}^T$$

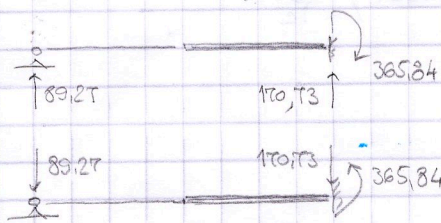
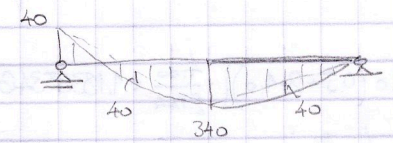
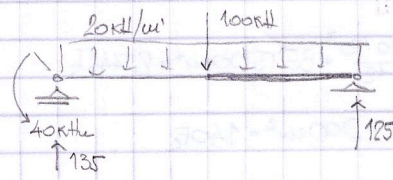
$$P_n^* = \begin{bmatrix} 1 & 2 \\ 0 & -100 \end{bmatrix}^T$$

$$S_n^* = \begin{bmatrix} 1 & 2 \\ 0 & -189.27 \end{bmatrix}^T$$

$$q_n^* = K_{nn}^{-1} S_n^*$$

$$q_n^* = \begin{bmatrix} 117 & 633,4484 & 16192,50351 \\ & & 97236 \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ -189,27 \end{bmatrix}$$

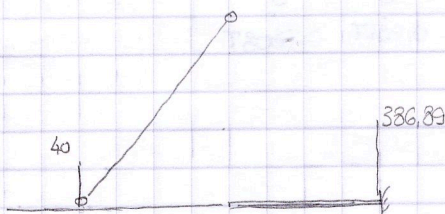
$$q_n^* = \begin{bmatrix} 0,000227498 & -0,0021261687 \end{bmatrix}^T$$

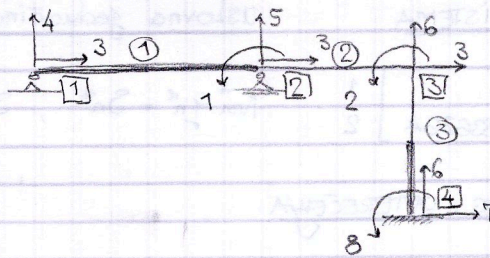
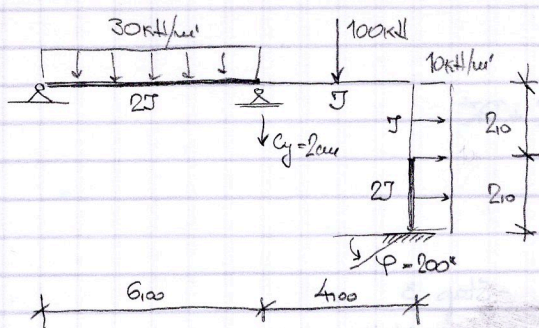


SILE NA KRAJEVIMA ŠTAPOVA

$$P_i = K_i T_i q_i^* - T_i Q_i^*$$

$$P_M = 93750 \begin{bmatrix} 1 & 2 & 5 & 6 & 7 \\ 7,0 & 0 & -7,0 & 0 & 0 \\ 0 & 0,0132 & 0 & -0,0132 & 0,1056 \\ -7,0 & 0 & 7,0 & 0 & 0 \\ 0 & -0,0132 & 0 & 0,0132 & -0,1056 \\ 0 & 0,1056 & 0 & -0,1056 & 0,84483 \end{bmatrix} \begin{bmatrix} 0,000227498 \\ -0,0021261687 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ -89,27 \\ 0 \\ -170,73 \\ 365,84 \end{bmatrix} = \begin{bmatrix} 149,30 \\ 86,64 \\ -149,30 \\ 173,36 \\ -386,89 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{matrix}$$





$b = 0.30m$ ;  $h = 0.60m$ ;  $E = 31500000 \text{ kN/m}^2$

	$l$	$\kappa$	$p$	$\lambda$	$\mu$	$J$
1	1	2	6.00	1	0	0.0108
2	2	3	4.00	1	0	0.0054
3	3	4	4.00	0	-1	

MATRICE KRUTOSTI ŠTAPOVA

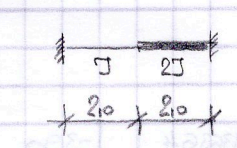
- Štap 1 (tipa „g“)

$$K_1 = K_1^* = \begin{bmatrix} \frac{3EJ}{p^3} & -\frac{3EJ}{p^3} & \frac{3EJ}{p^2} \\ -\frac{3EJ}{p^3} & \frac{3EJ}{p^3} & -\frac{3EJ}{p^2} \\ \frac{3EJ}{p^2} & -\frac{3EJ}{p^2} & \frac{3EJ}{p} \end{bmatrix} = \begin{bmatrix} 4725 & -4725 & 28350 \\ -4725 & 4725 & -28350 \\ 28350 & -28350 & 170100 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 1 \end{matrix}$$

- Štap 2 (tipa „k“)

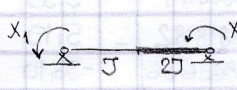
$$K_2 = K_2^* = \begin{bmatrix} \frac{12EJ}{p^3} & \frac{6EJ}{p^2} & -\frac{12EJ}{p^3} & \frac{6EJ}{p^2} \\ \frac{6EJ}{p^2} & \frac{4EJ}{p} & -\frac{6EJ}{p^2} & \frac{2EJ}{p} \\ -\frac{12EJ}{p^3} & -\frac{6EJ}{p^2} & \frac{12EJ}{p^3} & -\frac{6EJ}{p^2} \\ -\frac{6EJ}{p^2} & \frac{2EJ}{p} & -\frac{6EJ}{p^2} & \frac{4EJ}{p} \end{bmatrix} = \begin{bmatrix} 31893.75 & 63787.5 & -31893.75 & 63787.5 \\ 63787.5 & 170100 & -63787.5 & 85050 \\ -31893.75 & -63787.5 & 31893.75 & -63787.5 \\ -63787.5 & 85050 & -63787.5 & 170100 \end{bmatrix} \begin{matrix} 5 \\ 1 \\ 6 \\ 2 \end{matrix}$$

- Štap 3

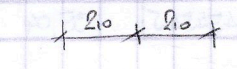


$J_c = J$

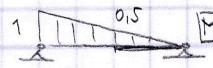
$$EJ_c \delta_{11} = \int_0^s M_1^2 \frac{J_c}{J} ds = \frac{1}{3} \cdot 0.5^2 \cdot \frac{2000}{2} + \frac{1}{6} \cdot [10 \cdot (2 \cdot 10 + 0.5) + 0.5 \cdot (10 + 2 \cdot 0.5)] \cdot 2000 = 1.25$$



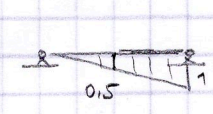
$$EJ_c \delta_{12} = \int_0^s M_1 M_2 \frac{J_c}{J} ds = \frac{1}{6} \cdot 0.5 \cdot (2 \cdot 0.5 + 10) \cdot \frac{2000}{2} - \frac{1}{6} \cdot 0.5 \cdot (2 \cdot 0.5 + 10) \cdot 2000 = -0.50$$



$$EJ_c \delta_{22} = \int_0^s M_2^2 \frac{J_c}{J} ds = \frac{1}{3} \cdot 0.5^2 \cdot 2000 + \frac{1}{6} \cdot [0.5 \cdot (2 \cdot 0.5 + 10) + 10 \cdot (0.5 + 2 \cdot 10)] \cdot \frac{2000}{2} = 0.75$$



matrica fleksibilnosti      bazna matrica krutosti



$$f = \frac{1}{EJ_c} \begin{bmatrix} 1.25 & -0.5 \\ -0.5 & 0.75 \end{bmatrix} \quad K_0 = f^{-1} = EJ_c \begin{bmatrix} 1.090909091 & 0.727272727 \\ 0.727272727 & 1.818181818 \end{bmatrix}$$

matrica zavrtanje

$$C = \begin{bmatrix} 1/E & 1 & -1/E & 0 \\ 1/E & 0 & -1/E & 1 \end{bmatrix} = \begin{bmatrix} 0.25 & 1 & -0.25 & 0 \\ 0.25 & 0 & -0.25 & 1 \end{bmatrix} \quad K_3 = C^T K_0 C = K_3^* = \begin{bmatrix} 46390.90908 & 77318.18181 & -46390.90908 & 108245.454526 \\ 77318.18181 & 185563.63636 & -77318.18181 & 123700.090909 \\ -46390.90908 & -77318.18181 & 46390.90908 & -108245.454526 \\ 108245.454526 & 123700.090909 & -108245.454526 & 309272.7272418 \end{bmatrix} \begin{matrix} 3 \\ 2 \\ 7 \\ 8 \end{matrix}$$

# MATRICA KRUTOSTI SISTEMA

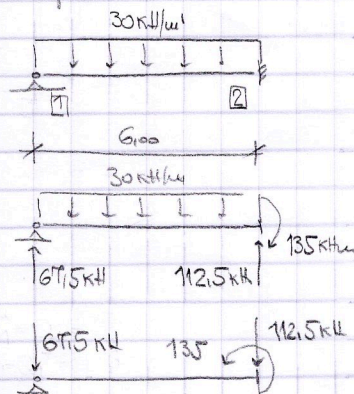
# USLOVNA JEDNAČINA

$$K_{nn} = \begin{bmatrix} 1 & 2 \\ 340200 & 85050 \\ 85050 & 355663,636364 \end{bmatrix} \begin{matrix} 1 \\ 2 \end{matrix}$$

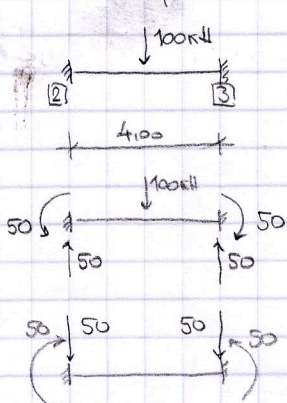
$$K_{nn} q_n^* = S_n^* ; S_n^* = Q_n^* + P_n^*$$

## VEKTOR EKIVALENTNOG OPTEREĆENJA

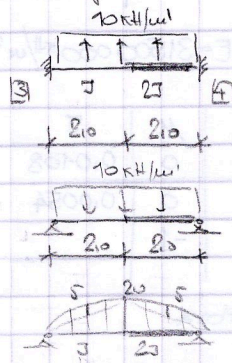
- step 1



- step 2



- step 3



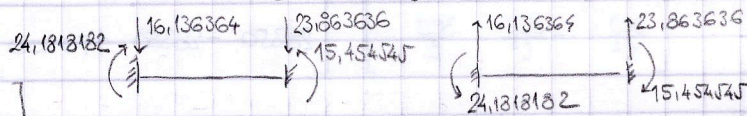
$$\begin{aligned} E J_c \delta_{10} &= \int_0^s M_1 M_0 \frac{J_c}{J} ds = \\ &= + \frac{1}{3} (1+0.5) \cdot 5 \cdot 2_0 + \\ &+ \frac{1}{6} (1_0 + 2 \cdot 0.5) \cdot 2_0 \cdot 2_0 + \\ &- \frac{1}{3} 0.5 \cdot 2_0 \cdot \frac{2_0}{2} + \\ &+ \frac{1}{3} \cdot 0.5 \cdot 5 \cdot \frac{2_0}{2} = +22.5 \\ E J_c \delta_{20} &= -\frac{1}{3} \cdot 0.5 \cdot 2_0 \cdot 2_0 - \end{aligned}$$

$$Q_1 = Q_1^* = \begin{bmatrix} -67.5 & -112.5 & 135 \end{bmatrix}^T \quad Q_2 = Q_2^* = \begin{bmatrix} -50 & -50 & -50 & 50 \end{bmatrix}^T$$

$$-\frac{1}{3} \cdot 0.5 \cdot 5 \cdot 2_0 - \frac{1}{6} 2_0 (2 \cdot 0.5 + 1_0) \cdot \frac{2_0}{2} - \frac{1}{3} (0.5 + 1_0) \cdot 5_0 \cdot \frac{2_0}{2} = -17.5$$

$$\begin{cases} 1.25x_1 - 0.5x_2 + 22.5 = 0 \\ -0.5x_1 + 0.75x_2 - 17.5 = 0 \end{cases} \quad \begin{cases} x_1 = -24.1818182 \\ x_2 = 15.454545 \end{cases}$$

$$Q_n^* = \begin{bmatrix} 85 & 74.1818182 \end{bmatrix}^T \quad P_n^* = 0$$



$$q_n^* = \begin{bmatrix} 0.000003126348663 & -0.000007476051151 \\ -0.000007476051151 & 0.0000230042046 \end{bmatrix} \begin{bmatrix} 85 \\ 74.1818182 \end{bmatrix}$$

$$q_n^* = \begin{bmatrix} 0.0002102809296 & 0.0001582883921 \end{bmatrix}^T$$

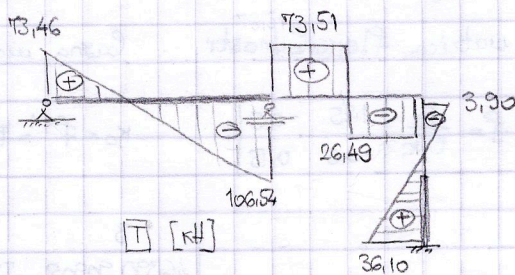
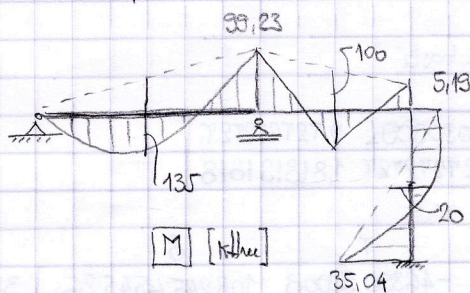
$$Q_3 = Q_3^* = \begin{bmatrix} 16.136364 & 24.1818182 & 23.863636 & -15.454545 \end{bmatrix}^T$$

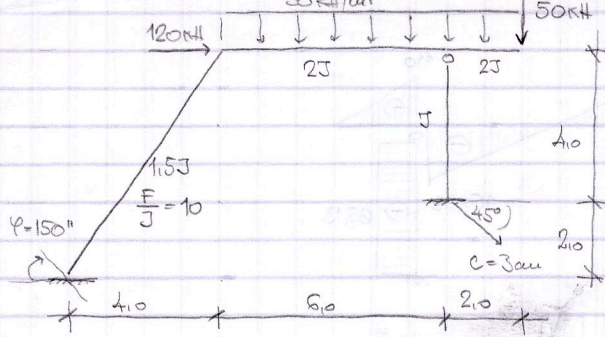
## SILE NA KRAJEVIMA STAPA $R_i = k_i q_i - Q_i$

$$R_1 = \begin{bmatrix} 4 & 5 & 1 \\ 4725 & -4725 & 28350 \\ -4725 & 4725 & -28350 \\ 28350 & -28350 & 170100 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0.0002102809296 \end{bmatrix} - \begin{bmatrix} -67.5 \\ -112.5 \\ 135 \end{bmatrix} = \begin{bmatrix} 73.46 \\ 106.54 \\ -39.23 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 1 \end{matrix}$$

$$R_2 = \begin{bmatrix} 5 & 1 & 6 & 2 \\ 31893.75 & 63787.5 & -31893.75 & 63787.5 \\ 63787.5 & 170100 & -63787.5 & 85050 \\ -31893.75 & -63787.5 & 31893.75 & -63787.5 \\ 63787.5 & 85050 & -63787.5 & 170100 \end{bmatrix} \begin{bmatrix} 0 \\ 0.0002102809296 \\ 0 \\ 0.0001582883921 \end{bmatrix} - \begin{bmatrix} -50 \\ -50 \\ -50 \\ 50 \end{bmatrix} = \begin{bmatrix} 73.51 \\ 99.23 \\ 26.49 \\ -5.19 \end{bmatrix} \begin{matrix} 5 \\ 1 \\ 6 \\ 2 \end{matrix}$$

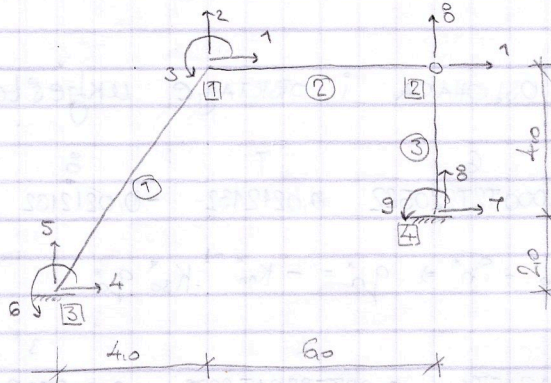
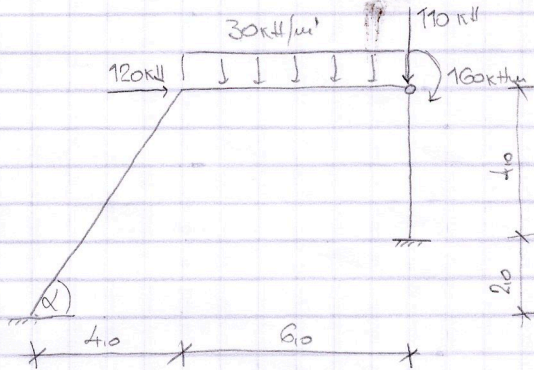
$$R_3 = \begin{bmatrix} 3 & 2 & 7 & 8 \\ 46390.90908 & 77318.18181 & -46390.90908 & 108245.454526 \\ 77318.18181 & 185563.636364 & -77318.18181 & 123709.090909 \\ -46390.90908 & -77318.18181 & 46390.90908 & -108245.454526 \\ 108245.454526 & 123709.090909 & -108245.454526 & 309272.7272418 \end{bmatrix} \begin{bmatrix} 0 \\ 0.0001582883921 \\ 0 \\ 0 \end{bmatrix} - \begin{bmatrix} 16.136364 \\ 24.1818182 \\ 23.863636 \\ -15.454545 \end{bmatrix} = \begin{bmatrix} -3.90 \\ 5.19 \\ -36.10 \\ 35.04 \end{bmatrix} \begin{matrix} 3 \\ 2 \\ 7 \\ 8 \end{matrix}$$





Pri bližina metoda deforamacije

$EJ = 100\ 000\ \text{kNm}^2$



Matrice krutosti stupova

- Step 1  $l_1 = 7.211\text{m}$

$$K_1 = \begin{bmatrix} \frac{EF}{L} & 0 & 0 & -\frac{EF}{L} & 0 & 0 \\ 0 & \frac{12EJ}{L^3} & \frac{6EJ}{L^2} & 0 & -\frac{12EJ}{L^3} & \frac{6EJ}{L^2} \\ 0 & \frac{6EJ}{L^2} & \frac{4EJ}{L} & 0 & -\frac{6EJ}{L^2} & \frac{2EJ}{L} \\ -\frac{EF}{L} & 0 & 0 & \frac{EF}{L} & 0 & 0 \\ 0 & -\frac{12EJ}{L^3} & -\frac{6EJ}{L^2} & 0 & \frac{12EJ}{L^3} & -\frac{6EJ}{L^2} \\ 0 & \frac{6EJ}{L^2} & \frac{2EJ}{L} & 0 & -\frac{6EJ}{L^2} & \frac{4EJ}{L} \end{bmatrix} = EJ \begin{bmatrix} 1.38675 & 0 & 0 & -1.38675 & 0 & 0 \\ 0 & 0.048003 & 0.173077 & 0 & -0.048003 & 0.173077 \\ 0 & 0.173077 & 0.83205 & 0 & -0.173077 & 0.416025 \\ -1.38675 & 0 & 0 & 1.38675 & 0 & 0 \\ 0 & -0.048003 & -0.173077 & 0 & 0.048003 & -0.173077 \\ 0 & 0.173077 & 0.416025 & 0 & -0.173077 & 0.83205 \end{bmatrix}$$

$$T_1 = \begin{bmatrix} \cos \alpha & \sin \alpha & 1 \\ -\sin \alpha & \cos \alpha & 0 \\ \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \end{bmatrix} = \begin{bmatrix} 0.5547 & 0.8320503 & 1 \\ -0.8320503 & 0.5547 & 0 \\ 0.5547 & 0.8320503 & 0 \\ -0.8320503 & 0.5547 & 0 \end{bmatrix}$$

$$K_1^* = T_1^T K_1 T_1 = EJ \begin{bmatrix} 0.459925 & 0.617883 & -0.1440088 & -0.459925 & -0.617883 & -0.1440088 & 4 \\ 0.617883 & 0.974828 & 0.0960058 & -0.617883 & -0.974828 & 0.0960058 & 5 \\ -0.1440088 & 0.0960058 & 0.83205 & 0.1440088 & -0.0960058 & 0.416025 & 6 \\ -0.459925 & -0.617883 & 0.1440088 & 0.459925 & 0.617883 & 0.1440088 & 1 \\ -0.617883 & -0.974828 & -0.0960058 & 0.617883 & 0.974828 & -0.0960058 & 2 \\ -0.1440088 & 0.0960058 & 0.416025 & 0.1440088 & -0.0960058 & 0.83205 & 3 \end{bmatrix}$$

- Step 2  $l_2 = 6.00\text{m}$

$$K_2 = \frac{EJ}{L^3} \begin{bmatrix} 3 & 3L & -3 \\ 3L & 3L^2 & -3L \\ -3 & -3L & 3 \end{bmatrix} = EJ \begin{bmatrix} 0.027778 & 0.16667 & -0.027778 \\ 0.16667 & 1.0 & -0.16667 \\ -0.027778 & -0.16667 & 0.027778 \end{bmatrix} = K_2^*$$

- Step 3  $l_3 = 4.00\text{m}$

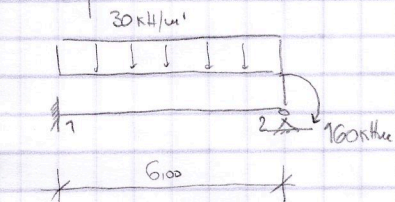
$$K_3 = \frac{EJ}{L^3} \begin{bmatrix} 3 & -3 & 3L \\ -3 & 3 & -3L \\ 3L & -3L & 3L^2 \end{bmatrix} = EJ \begin{bmatrix} 0.046875 & -0.046875 & 0.1875 \\ -0.046875 & 0.046875 & -0.1875 \\ 0.1875 & -0.1875 & 0.75 \end{bmatrix} = T = K_3^*$$

(1)

$$K^* = EJ \begin{bmatrix} 1 & 2 & 3 \\ 0,5068 & 0,617883 & 0,1440088 & -0,459925 & -0,617883 & 0,1440088 & -0,046875 & 0 & 0,1875 \\ & 1,002606 & 0,0706642 & -0,617883 & -0,974828 & -0,0960058 & 0 & -0,027728 & 0 \\ & & 1,83205 & -0,1440088 & 0,0960058 & 0,416025 & 0 & -0,16687 & 0 \end{bmatrix}$$

Vektor ekvivalentnog opterećenja

- step 2



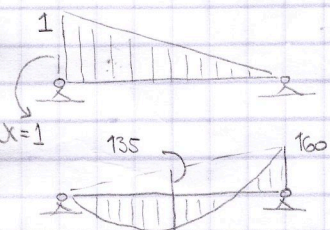
$$EJ \delta_{11}^0 = \frac{1}{3} \cdot 1^2 \cdot 6_{10} = 2_{10}$$

$$EJ \delta_{10}^0 = \frac{1}{6} \cdot 1 \cdot 160 \cdot 6_{10} - \frac{1}{3} \cdot 1 \cdot 135 \cdot 6_{10} = -110$$

$$X = \frac{-EJ \delta_{10}^0}{EJ \delta_{11}^0} = \frac{110}{2} = 55 \text{ kN}$$

$$T_1 = \frac{30 \cdot 6_{10}}{2} - \frac{160 - 55}{6_{10}} = 172,5 \text{ kN}$$

$$T_2 = -\frac{30 \cdot 6_{10}}{2} - \frac{160 - 55}{6_{10}} = -107,5 \text{ kN}$$

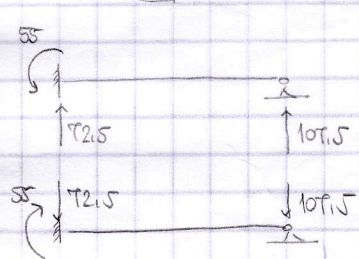


$$Q_2 = Q_2^* = \begin{bmatrix} 2 & 3 & 8 \\ -172,5 & -55 & -107,50 \end{bmatrix}^T$$

$$Q^* = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 & 9 \\ 0 & -172,50 & -55 & 0 & 0 & 0 & 0 & -107,50 & 0 \end{bmatrix}$$

$$P^* = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 & 9 \\ 120 & 0 & 0 & 0 & 0 & 0 & 0 & -110 & 0 \end{bmatrix}$$

$$S_n^* = Q_n^* + P_n^* = \begin{bmatrix} 1 & 2 & 3 \\ 120 & -172,50 & -55 \end{bmatrix}$$



Ustavne jednačine - proračun nepoznatih generalisanih pomeranja

$$K_{nn}^* q_n^* = S_n^* \Rightarrow q_n^* = K_{nn}^{*-1} S_n^*$$

$$q_n^* = \begin{bmatrix} 1 & 2 & 3 \\ 1389,52908 & -921,336926 & -103,708348 \end{bmatrix}^T \cdot \frac{1}{EJ}$$

Site na krajevima štapova  $R_i = K_i T_i q_i^* - T_i Q_i^*$

step 1

$$q_1^* = \begin{bmatrix} 4 & 5 & 6 & 1 & 2 & 3 \\ 0 & 0 & 0 & 1389,52908 & -921,336926 & -103,708348 \end{bmatrix}^T \cdot \frac{1}{EJ}; \quad q_2^* = \begin{bmatrix} 2 & 3 & 8 \\ -921,336926 & -103,708348 & 0 \end{bmatrix}^T \cdot \frac{1}{EJ}$$

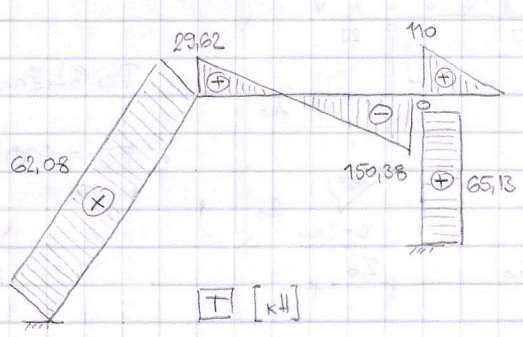
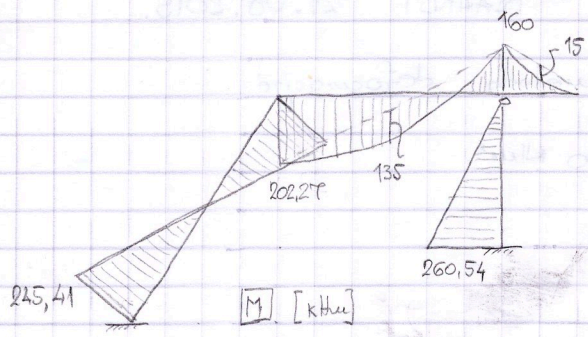
$$R_1 = \begin{bmatrix} -5,79 & 4 \\ 62,08 & 5 \\ 245,41 & 6 \\ 5,79 & 1 \\ -62,08 & 2 \\ 202,27 & 3 \end{bmatrix}$$

$$R_2 = \begin{bmatrix} 29,62 & 2 \\ -202,27 & 3 \\ 150,38 & 8 \end{bmatrix}$$

$$R_3 = \begin{bmatrix} 65,13 & 1 \\ -65,13 & 7 \\ 260,54 & 3 \end{bmatrix}$$

$$q_3^* = \begin{bmatrix} 1 & 7 & 9 \\ 1389,52908 & 0 & 0 \end{bmatrix}^T \cdot \frac{1}{EJ}$$

2



Pomeranje OSLOHACA i ORBITAJE ukjestejaja

$$q_0^* = \begin{bmatrix} 4 & 5 & 6 & 7 & 8 & 9 \\ 0 & 0 & 0,000727220522 & 0,0212132 & -0,0212132 & 0 \end{bmatrix}^T$$

$$K_{nn}^* q_n^* + K_{so}^* q_0^* = S_n^* \Rightarrow q_n^* = -K_{nn}^{-1} K_{so}^* q_0^*$$

$$q_n^* = \begin{bmatrix} 1 & 2 & 3 \\ 0,0117752284571 & -0,007582615237 & -0,002728125893 \end{bmatrix}^T$$

Side na krajenua štapava  $R_i = K_i T_i q_i^*$

$$q_1^* = \begin{bmatrix} 4 & 5 & 6 & 1 & 2 & 3 \\ 0 & 0 & 0,000727220522 & 0,0117752284571 & -0,007582615237 & -0,002728125893 \end{bmatrix}^T$$

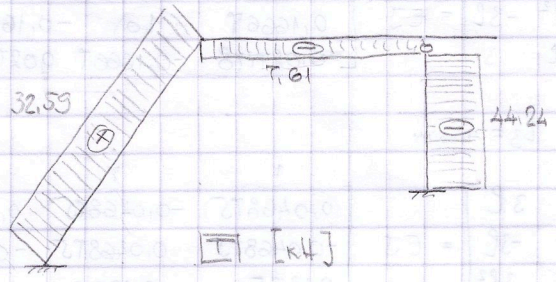
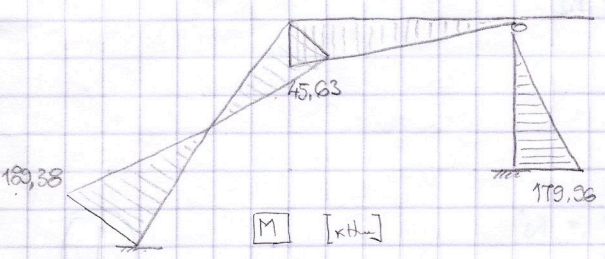
$$R_1 = \begin{bmatrix} -30,87 & 4 \\ 32,59 & 5 \\ 189,38 & 6 \\ 30,87 & 1 \\ -32,59 & 2 \\ 45,63 & 3 \end{bmatrix}$$

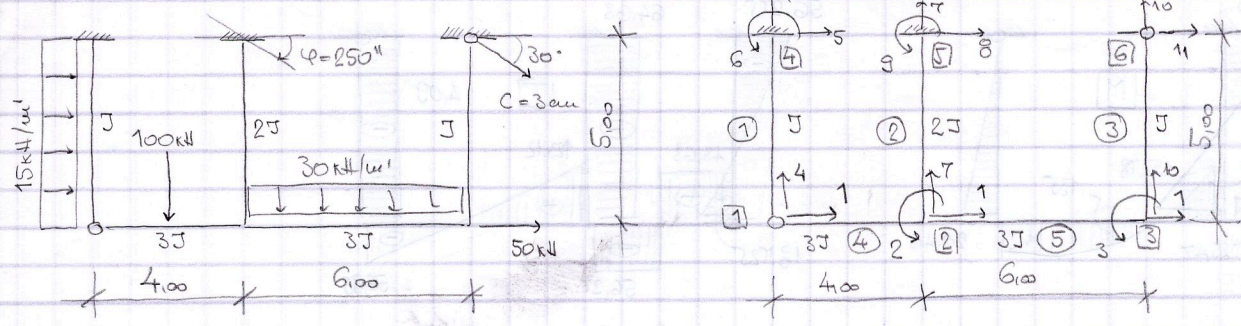
$$q_2^* = \begin{bmatrix} 2 & 3 & 8 \\ -0,007582615237 & -0,002728125893 & -0,0212132 \end{bmatrix}^T$$

$$R_2 = \begin{bmatrix} -7,61 & 2 \\ -45,63 & 3 \\ 7,61 & 8 \end{bmatrix}$$

$$q_3^* = \begin{bmatrix} 1 & 7 & 9 \\ 0,0117752284571 & 0,0212132 & 0 \end{bmatrix}^T$$

$$R_3 = \begin{bmatrix} -44,24 & 1 \\ 44,24 & 7 \\ -116,96 & 9 \end{bmatrix}$$





Matrice krutosti stupova

- Step 1  $l = 5,00 \text{ m}$

$$K_1 = \begin{bmatrix} \frac{3EJ}{l^3} & \frac{3EJ}{l^2} & -\frac{3EJ}{l^3} \\ \frac{3EJ}{l^2} & \frac{3EJ}{l} & -\frac{3EJ}{l^2} \\ -\frac{3EJ}{l^3} & -\frac{3EJ}{l^2} & \frac{3EJ}{l^3} \end{bmatrix} = EJ \begin{bmatrix} 5 & 6 & 1 \\ 0,024 & 0,12 & -0,024 \\ 0,12 & 0,6 & -0,12 \\ -0,024 & -0,12 & 0,024 \end{bmatrix} = K_1^* \begin{matrix} 5 \\ 6 \\ 1 \end{matrix}$$

- Step 2  $l = 5,00 \text{ m}$

$$K_2 = \begin{bmatrix} \frac{12EJ}{l^3} & \frac{6EJ}{l^2} & -\frac{12EJ}{l^3} & \frac{6EJ}{l^2} \\ \frac{6EJ}{l^2} & \frac{4EJ}{l} & -\frac{6EJ}{l^2} & \frac{2EJ}{l} \\ -\frac{12EJ}{l^3} & -\frac{6EJ}{l^2} & \frac{12EJ}{l^3} & -\frac{6EJ}{l^2} \\ \frac{6EJ}{l^2} & \frac{2EJ}{l} & -\frac{6EJ}{l^2} & \frac{4EJ}{l} \end{bmatrix} = EJ \begin{bmatrix} 8 & 9 & 1 & 2 \\ 0,192 & 0,48 & -0,192 & 0,48 \\ 0,48 & 1,60 & -0,48 & 0,80 \\ -0,192 & -0,48 & 0,192 & -0,48 \\ 0,48 & 0,80 & -0,48 & 1,60 \end{bmatrix} = K_2^* \begin{matrix} 8 \\ 9 \\ 1 \\ 2 \end{matrix}$$

- Step 3  $l = 5,00 \text{ m}$

$$K_3 = \begin{bmatrix} \frac{3EJ}{l^3} & -\frac{3EJ}{l^3} & \frac{3EJ}{l^2} \\ -\frac{3EJ}{l^3} & \frac{3EJ}{l^3} & -\frac{3EJ}{l^2} \\ \frac{3EJ}{l^2} & -\frac{3EJ}{l^2} & \frac{3EJ}{l} \end{bmatrix} = EJ \begin{bmatrix} 11 & 1 & 3 \\ 0,024 & -0,024 & 0,12 \\ -0,024 & 0,024 & -0,12 \\ 0,12 & -0,12 & 0,60 \end{bmatrix} = K_3^* \begin{matrix} 11 \\ 1 \\ 3 \end{matrix}$$

- Step 4  $l = 4,00 \text{ m}$

$$K_4 = \begin{bmatrix} \frac{3EJ}{l^3} & -\frac{3EJ}{l^3} & \frac{3EJ}{l^2} \\ -\frac{3EJ}{l^3} & \frac{3EJ}{l^3} & -\frac{3EJ}{l^2} \\ \frac{3EJ}{l^2} & -\frac{3EJ}{l^2} & \frac{3EJ}{l} \end{bmatrix} = EJ \begin{bmatrix} 4 & 7 & 2 \\ 0,140625 & -0,140625 & 0,5625 \\ -0,140625 & 0,140625 & -0,5625 \\ 0,5625 & -0,5625 & 2,25 \end{bmatrix} = K_4^* \begin{matrix} 4 \\ 7 \\ 2 \end{matrix}$$

- Step 5  $l = 6,00 \text{ m}$

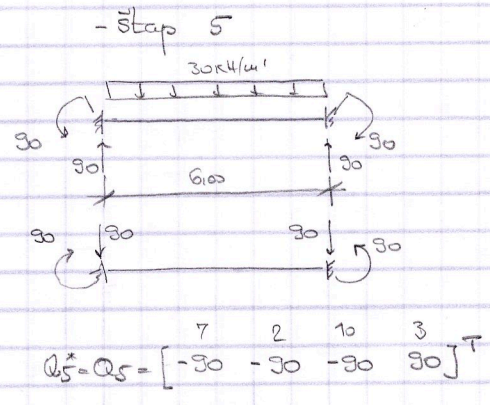
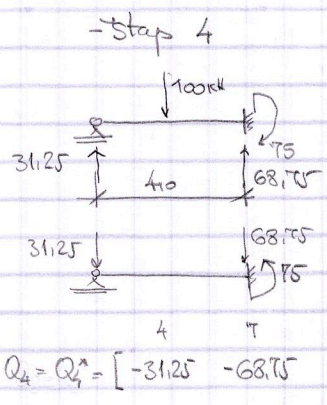
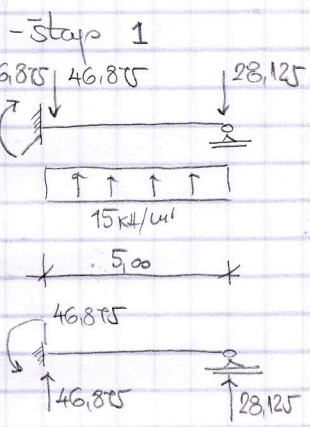
$$K_5 = \begin{bmatrix} \frac{12EJ}{l^3} & \frac{6EJ}{l^2} & -\frac{12EJ}{l^3} & \frac{6EJ}{l^2} \\ \frac{6EJ}{l^2} & \frac{4EJ}{l} & -\frac{6EJ}{l^2} & \frac{2EJ}{l} \\ -\frac{12EJ}{l^3} & -\frac{6EJ}{l^2} & \frac{12EJ}{l^3} & -\frac{6EJ}{l^2} \\ \frac{6EJ}{l^2} & \frac{2EJ}{l} & -\frac{6EJ}{l^2} & \frac{4EJ}{l} \end{bmatrix} = EJ \begin{bmatrix} 7 & 2 & 10 & 3 \\ 0,166667 & 0,50 & -0,166667 & 0,50 \\ 0,50 & 2,0 & -0,50 & 1,0 \\ -0,166667 & -0,50 & 0,166667 & -0,50 \\ 0,50 & 1,0 & -0,50 & 2,0 \end{bmatrix} = K_5^* \begin{matrix} 7 \\ 2 \\ 10 \\ 3 \end{matrix}$$

1



$$K^* = EJ \begin{bmatrix} 0,24 & -0,48 & -0,12 & 0 & -0,024 & -0,12 & 0 & -0,192 & -0,48 & 0 & -0,024 \\ -0,48 & 5,85 & 1,0 & 0,5625 & 0 & 0 & -0,0625 & 0,48 & 0,80 & -0,50 & 0 \\ -0,12 & 1,0 & 2,60 & 0 & 0 & 0 & 0,50 & 0 & 0 & -0,50 & 0,12 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & -0,024 & -0,12 & 0 & -0,192 & -0,48 & 0 & -0,024 & -0,48 & 0 & -0,024 \\ 0,5625 & 0 & 0 & -0,0625 & 0,48 & 0,80 & -0,50 & 0 & 0,80 & -0,50 & 0 \\ 0 & 0 & 0 & 0,50 & 0 & 0 & -0,50 & 0,12 & 0 & -0,50 & 0,12 \end{bmatrix}$$

VEKTOR EKIVALENTNOG OPTEREĆENJA



$$Q_1^* = Q_1 = \begin{bmatrix} 46,875 & 46,875 & 28,125 \end{bmatrix}^T$$

$$Q^* = \begin{bmatrix} 28,125 & -15 & 30 & -31,25 & 46,875 & 46,875 & -158,75 & 0 & 0 & -30 & 0 \end{bmatrix}^T$$

$$P^* = \begin{bmatrix} 50 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}^T$$

$$S_n^* = Q_n^* + P_n^* = \begin{bmatrix} 28,125 & -15 & 30 \end{bmatrix}^T + \begin{bmatrix} 50 & 0 & 0 \end{bmatrix}^T = \begin{bmatrix} 78,125 & -15 & 30 \end{bmatrix}^T$$

Uslovne jednačine - proračun nepoznatih parametara pomeranja

$$K_{nn}^* q_n^* = S_n^* \Rightarrow q_n^* = K_{nn}^{*-1} S_n^*$$

$$q_n^* = \frac{1}{EJ} \begin{bmatrix} 0,24 & -0,48 & -0,12 \\ -0,48 & 5,85 & 1,0 \\ -0,12 & 1,0 & 2,60 \end{bmatrix}^{-1} \begin{bmatrix} 78,125 \\ -15 \\ 30 \end{bmatrix} = \frac{1}{EJ} \begin{bmatrix} 391,6576 \\ 22,0119 \\ 44,2258 \end{bmatrix}$$

Sile na krajevima šrafova  $R_i = k_i T_i q_i^* - T_i Q_i^*$

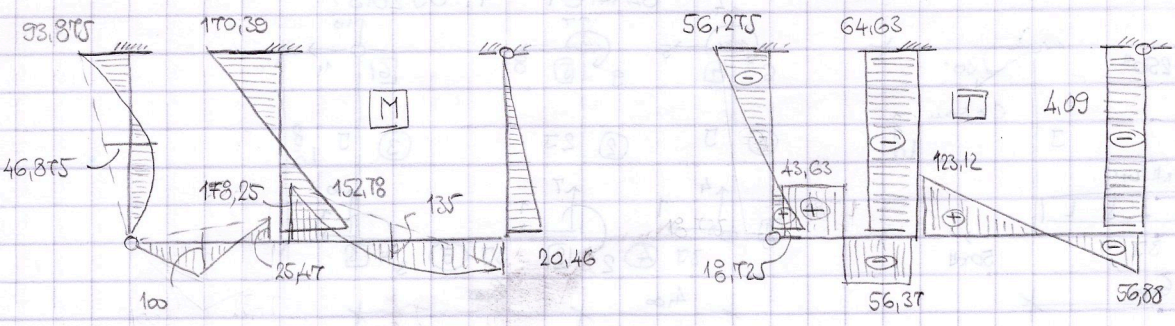
$$q_1^* = \begin{bmatrix} 0 \\ 0 \\ 391,6576 \end{bmatrix} \frac{1}{EJ} \quad R_1 = \begin{bmatrix} -56,275 \\ -93,875 \\ -18,125 \end{bmatrix}$$

$$q_2^* = \begin{bmatrix} 0 \\ 0 \\ 391,6576 \\ 22,0119 \end{bmatrix} \frac{1}{EJ} \quad R_2 = \begin{bmatrix} -64,63 \\ -170,39 \\ 64,63 \\ -152,78 \end{bmatrix}$$

$$q_3^* = \begin{bmatrix} 0 \\ 391,6576 \\ 44,2258 \end{bmatrix} \frac{1}{EJ} \quad R_3 = \begin{bmatrix} -4,09 \\ 4,09 \\ -20,46 \end{bmatrix}$$

$$q_4^* = \begin{bmatrix} 0 \\ 0 \\ 22,0119 \end{bmatrix} \frac{1}{EJ} \quad R_4 = \begin{bmatrix} 43,63 \\ 56,37 \\ -25,47 \end{bmatrix}$$

$$q_5^* = \begin{bmatrix} 0 \\ 22,0119 \\ 0 \\ 44,2258 \end{bmatrix} \frac{1}{EJ} \quad R_5 = \begin{bmatrix} 123,12 \\ 178,25 \\ 56,88 \\ 20,46 \end{bmatrix}$$



Pomeranje oslonaca i obznanje ukloštenja

$$q_0^* = [0 \ 0 \ 0 \ 0 \ 0 \ -0.001212034203 \ -0.015 \ 0.025380762]^T$$

$$K_{nn}^* q_n^* + K_{no}^* q_0^* = S_n^* \Rightarrow q_n^* = -K_{nn}^{-1} K_{no}^* q_0^*$$

$$q_n^* = [-0.003212147701256 \ -0.000702644618211 \ -0.003361732517669]^T$$

Sile na krajevima štapova  $R_i = K_i T_i q_i^*$  Vred je:  $J = \frac{1}{1000} m^4$   $EJ = 30000 kNm^2$

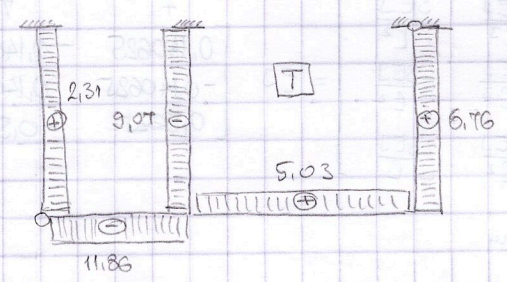
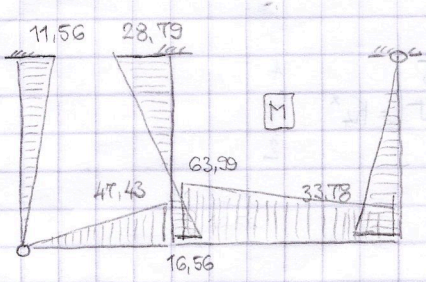
$$q_1^* = \begin{bmatrix} 0 \\ 0 \\ -0.00321215 \end{bmatrix}; R_1 = EJ \begin{bmatrix} 0.00077001545 \\ 0.0003854577 \\ -0.00077001545 \end{bmatrix} = \begin{bmatrix} 2.31 \\ 11.56 \\ -2.31 \end{bmatrix} \begin{matrix} 5 \\ 6 \\ 1 \end{matrix}$$

$$q_2^* = \begin{bmatrix} 0 \\ -0.001212034 \\ -0.00321215 \\ -0.000702645 \end{bmatrix}; R_2 = EJ \begin{bmatrix} -0.00030231312 \\ -0.0009595384 \\ 0.00030231312 \\ -0.0005520272 \end{bmatrix} = \begin{bmatrix} -9.07 \\ -28.79 \\ 9.07 \\ -16.56 \end{bmatrix} \begin{matrix} 8 \\ 9 \\ 1 \\ 2 \end{matrix}$$

$$q_3^* = \begin{bmatrix} 0.025380762 \\ -0.00321215 \\ -0.0033617 \end{bmatrix}; R_3 = EJ \begin{bmatrix} 0.000225221931 \\ -0.000225221931 \\ 0.001126109654 \end{bmatrix} = \begin{bmatrix} 6.76 \\ -6.76 \\ 33.78 \end{bmatrix} \begin{matrix} 11 \\ 1 \\ 3 \end{matrix}$$

$$q_4^* = \begin{bmatrix} 0 \\ 0 \\ -0.000702644 \end{bmatrix}; R_4 = EJ \begin{bmatrix} -0.0003952376 \\ 0.0003952376 \\ -0.0015809504 \end{bmatrix} = \begin{bmatrix} -11.86 \\ 11.86 \\ -47.43 \end{bmatrix} \begin{matrix} 4 \\ 7 \\ 2 \end{matrix}$$

$$q_5^* = \begin{bmatrix} 0 \\ -0.000702645 \\ -0.015 \\ -0.00336173 \end{bmatrix}; R_5 = EJ \begin{bmatrix} 0.000167816432 \\ 0.00213297824 \\ -0.000167816432 \\ -0.00126109653 \end{bmatrix} = \begin{bmatrix} 5.03 \\ 63.99 \\ -5.03 \\ -33.78 \end{bmatrix} \begin{matrix} 7 \\ 2 \\ 10 \\ 3 \end{matrix}$$



$t_0 = 5^\circ\text{C}, t_{in} = -5^\circ\text{C}$   
 $\alpha_t = 10^{-5}$

Step	i	K	j	$\mu$	$\rho$	EJ	EF
1	3	1	1	0	5,00	27000	
2	1	2	0,80	-0,60	5,00	13500	1800000
3	2	4	1	0	7,00	20250	
4	2	5	0	-1	5,00	27000	

$E = 3 \cdot 10^7 \text{ kN/m}^2; b/h_e = 20/30 \text{ cm}$   
 $J = J_c = 4,5 \cdot 10^{-4} \text{ m}^4 \quad F = F_c = 6 \cdot 10^{-2} \text{ m}^2$   
 $1,5J \rightarrow h_e = 34,34 \text{ cm} \rightarrow J = 6,15 \cdot 10^{-4} \text{ m}^4$   
 $F = 6,868 \cdot 10^{-2} \text{ m}^2$   
 $2J \rightarrow h_e = 31,80 \text{ cm} \rightarrow J = 9 \cdot 10^{-4} \text{ m}^4$   
 $F = 7,96 \cdot 10^{-2} \text{ m}^2$

**- Step 1**

$$K_1^* = K_1 = \begin{bmatrix} \frac{3EJ}{P^3} & -\frac{3EJ}{P^3} & \frac{3EJ}{P^2} \\ \frac{3EJ}{P^3} & -\frac{3EJ}{P^3} & \frac{3EJ}{P^2} \\ \frac{3EJ}{P^2} & -\frac{3EJ}{P^2} & \frac{3EJ}{P} \end{bmatrix} = \begin{bmatrix} 5 & 2 & 3 \\ 648 & -648 & 3240 \\ 16200 & -16200 & 5 \end{bmatrix} \quad K_2 = \begin{bmatrix} \frac{EF}{P} & 0 & -\frac{EF}{P} & 0 \\ \frac{12EJ}{P^3} & \frac{6EJ}{P^2} & 0 & -\frac{12EJ}{P^3} & \frac{6EJ}{P^2} \\ 0 & 0 & -\frac{6EJ}{P^2} & \frac{2EJ}{P} & 0 \\ \frac{4EJ}{P} & 0 & -\frac{6EJ}{P^2} & \frac{2EJ}{P} & 0 \\ EF & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ \frac{12EJ}{P^3} & -\frac{6EJ}{P^2} & 0 & 0 & \frac{4EJ}{P} \end{bmatrix}$$

$K_2 = \begin{bmatrix} 4 & 2 & 3 & 6 & 7 & 1 \\ 360000 & 0 & 0 & -360000 & 0 & 0 \\ 0 & 1296 & 3240 & 0 & -1296 & 3240 \\ 0 & 3240 & 10800 & 0 & -3240 & 5400 \\ -360000 & 0 & 0 & 360000 & 0 & 0 \\ 0 & -1296 & -3240 & 0 & 1296 & -3240 \\ 0 & 3240 & 5400 & 0 & -3240 & 10800 \end{bmatrix} \quad T_2 = \begin{bmatrix} 0,80 & -0,60 \\ 0,60 & 0,80 \\ & & 1 \\ & & & 0,80 & -0,60 \\ & & & 0,60 & 0,80 \\ & & & & & 1 \end{bmatrix}$ 

$K_3^* = K_3 = \begin{bmatrix} \frac{3EJ}{P^3} & \frac{3EJ}{P^2} & -\frac{3EJ}{P^3} \\ \frac{3EJ}{P^2} & -\frac{3EJ}{P^2} & \frac{3EJ}{P} \\ \frac{3EJ}{P^3} & -\frac{3EJ}{P^2} & \frac{3EJ}{P} \end{bmatrix} = \begin{bmatrix} 7 & 1 & 8 \\ 177,114 & 1239,196 & -157,114 \\ 8678,571 & -1239,196 & 177,114 \end{bmatrix}$ 

$K_4 = K_4^* = \begin{bmatrix} 6 & 1 & 9 & 10 \\ 2592 & 6480 & -2592 & 6480 \\ & 21600 & -6480 & 10800 \\ & & 2592 & -6480 \\ & & & 21600 \end{bmatrix}$ 

$K_5^* = K_5 = \begin{bmatrix} 1 & 2 & 3 \\ 41078,571 & 2592 & 5400 \\ & 131077,44 & -648 \\ & & 27000 \end{bmatrix}$

$EJ \delta_{11}^* = \frac{1}{3} \cdot 10^2 \cdot 5 = 1667$   
 $EJ \delta_{10}^* = \frac{1}{6} \cdot 10 \cdot 5 \cdot 5 - \frac{1}{3} \cdot 10 \cdot 2.5 \cdot 5 = -41.91667$   
 $X = -\frac{EJ \delta_{10}^*}{EJ \delta_{11}^*} = 28.75 \text{ kNm}$

$Q_1 = Q_1^* = [-20.25 \quad -29.75 \quad 28.75]^T$

$3PP_{16} = 26.25 \text{ kNm}$

$Q_3 = Q_3^* = [-13.75 \quad -26.25 \quad -6.25]^T$

$Q_4 = Q_4^* = \begin{bmatrix} 12.50 \\ 10.4167 \\ 12.50 \\ -10.4167 \end{bmatrix}$

$Q_5^* = [-15.8333 \quad -29.75 \quad 28.75]^T \quad P_5^* = \vec{0} \quad ; \quad S_5^* = Q_5^* + P_5^*$

$K_{55}^* q_5^* = S_5^* \Rightarrow q_5^* = K_{55}^{-1} \cdot S_5^* \Rightarrow q_5^* = \begin{bmatrix} -0.000525257075583 & -0.000210810247467 & 0.001164806551132 \end{bmatrix}^T$

$P_i = K_i \cdot q_i - Q_i = K_i \cdot T_i q_i^* - T_i Q_i^*$

$R_1 = \begin{bmatrix} 648 & -648 & 3240 \\ & 648 & -3240 \\ & & 16200 \end{bmatrix} \begin{bmatrix} 0 \\ -0.00021082 \\ 0.00116480655 \end{bmatrix} - \begin{bmatrix} -20.25 \\ -29.75 \\ 28.75 \end{bmatrix} = \begin{bmatrix} 24.16 \\ 25.84 \\ -9.20 \end{bmatrix}$

$R_2 = \begin{bmatrix} 360000 & 0 & 0 & -360000 & 0 & 0 \\ & 1296 & 3240 & 0 & -1296 & 3240 \\ & & 10800 & 0 & -3240 & 5400 \\ & & & 360000 & 0 & 0 \\ & & & & 1296 & -3240 \\ & & & & & 10800 \end{bmatrix} \begin{bmatrix} 0.80 & -0.60 \\ 0.60 & 0.80 \\ & 0.80 & -0.60 \\ & & 0.60 & 0.80 \end{bmatrix} \begin{bmatrix} 0 \\ -0.00021082 \\ 0.00116480655 \\ 0 \\ 0 \\ -0.0005252571 \end{bmatrix} = \begin{bmatrix} 45.54 \\ 1.85 \\ 9.20 \\ -45.54 \\ -1.85 \\ 0.071 \end{bmatrix}$

$R_3 = \begin{bmatrix} 177,114 & 1239,796 & -177,114 \\ & 8648,511 & -1239,796 \\ & & 177,114 \end{bmatrix} \begin{bmatrix} 0 \\ -0.0005252571 \\ 0 \end{bmatrix} - \begin{bmatrix} -13.75 \\ -26.25 \\ -6.25 \end{bmatrix} = \begin{bmatrix} 13,10 \\ 21,69 \\ 6,90 \end{bmatrix}$

$R_4 = \begin{bmatrix} 2592 & 6480 & -2592 & 6480 \\ & 21600 & -6480 & 10800 \\ & & 2592 & -6480 \\ & & & 21600 \end{bmatrix} \begin{bmatrix} 0 \\ -0.0005252571 \\ 0 \\ 0 \end{bmatrix} - \begin{bmatrix} 12.50 \\ 10.4167 \\ 12.50 \\ -10.4167 \end{bmatrix} = \begin{bmatrix} -15,30 \\ -21,76 \\ -9,10 \\ 4,74 \end{bmatrix}$

Utjecaj temperaturne razlike  $t_0 = 5^\circ\text{C}$   $t_1 = -5^\circ\text{C}$ ;  $t_0$ ;  $\Delta t = 10^\circ\text{C}$

$$Q_2^T = EJ \alpha \frac{\Delta t}{h} [0 \ 1 \ 0 \ -1] = 13500 \cdot 10^{-5} \cdot \frac{10}{930} [0 \ 1 \ 0 \ -1] = [0 \ 4,50 \ 0 \ -4,50]$$

$$Q_2^* = T_2^T Q_2 = [0 \ 0 \ 4,50 \ 0 \ 0 \ -4,50]$$

$$Q_3 = Q_3^* = 1,50 EJ \alpha \frac{\Delta t}{h} \left[ \frac{1}{l} \ 1 \ -\frac{1}{l} \right] = 1,50 \cdot 20250 \cdot 10^{-5} \cdot \frac{10}{0,3434} \left[ \frac{1}{7,0} \ 1 \ -\frac{1}{7,0} \right] = [1,264 \ 8,845 \ -1,264]$$

$$Q_3^* = [4,345 \ 0 \ 4,50]$$

$$K_{SS} q_s^* = Q_3^* \Rightarrow q_s^* = K_{SS}^{-1} Q_3^* = [0,086193795140597 \ -0,000365841670515 \ 0,42404727438453] \cdot 10^{-3}$$

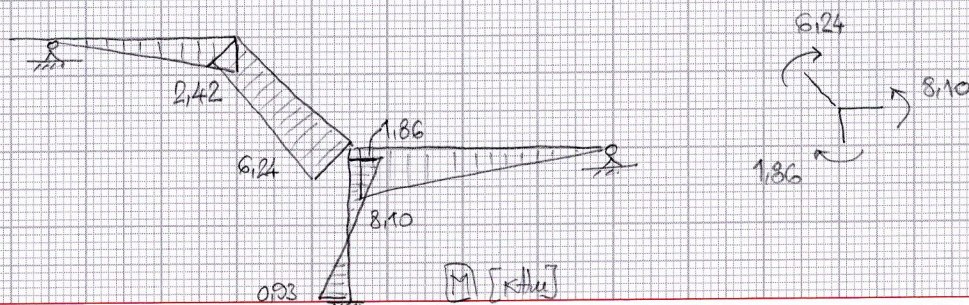
$$R_i = k_i q_i - Q_i = K T_i q_i^* - T_i Q_i^*$$

$$R_1 = \begin{bmatrix} 5 & 2 & 3 \\ 648 & -648 & 3240 \\ & 648 & -3240 \\ 15'' & & 16200 \end{bmatrix} \begin{bmatrix} 0 \\ -0,000365842 \\ 0,1494047274 \end{bmatrix} = \begin{bmatrix} 0,48 \\ -0,48 \\ 2,42 \end{bmatrix}$$

$$R_2 = \begin{bmatrix} 360000 & 0 & 0 & -360000 & 0 & 0 \\ 0 & 1296 & 3240 & 0 & -1296 & 3240 \\ 0 & 3240 & 10800 & 0 & -3240 & 5400 \\ -360000 & 0 & 0 & 360000 & 0 & 0 \\ 0 & -1296 & -3240 & 0 & 1296 & -3240 \\ 0 & 3240 & 5400 & 0 & -3240 & 10800 \end{bmatrix} \begin{bmatrix} 0,80 & -0,60 \\ 0,60 & 0,80 \\ 0,80 & -0,60 \\ 0,00 & 0,80 \end{bmatrix} = \begin{bmatrix} 0 \\ -0,000365842 \\ 0,1494047274 \\ 0 \\ 0 \\ 0,086193795 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 4,50 \\ 0 \\ 0 \\ -4,50 \end{bmatrix} = \begin{bmatrix} 0,21 \\ 0,76 \\ -2,42 \\ -0,21 \\ -0,76 \\ 6,24 \end{bmatrix}$$

$$R_3 = \begin{bmatrix} 177,114 & 1239,796 & -177,114 \\ & 8648,511 & -1239,796 \\ 15'' & & 177,114 \end{bmatrix} \begin{bmatrix} 0 \\ 0,0861937951 \\ 0 \end{bmatrix} = \begin{bmatrix} 1,264 \\ 8,845 \\ -1,264 \end{bmatrix} = \begin{bmatrix} -1,16 \\ -8,10 \\ 1,16 \end{bmatrix}$$

$$R_4 = \begin{bmatrix} 6 & 1 & 9 & 10 \\ 2592 & 6480 & -2592 & 6480 \\ & 21600 & -6480 & 10800 \\ & & 2592 & -6480 \\ & & & 21600 \end{bmatrix} \begin{bmatrix} 0 \\ 0,0861937951 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0,56 \\ 1,86 \\ -0,56 \\ 0,93 \end{bmatrix}$$



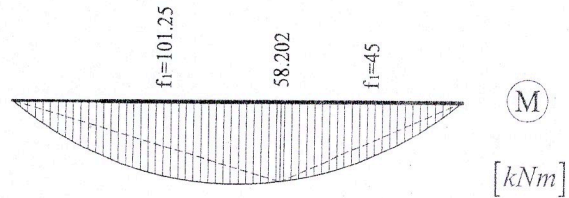
3

-štap 1:

$$q_i^* = \frac{1}{EI} \begin{bmatrix} 0 \\ 455.5224 \\ -241.9294 \\ 0 \\ 0 \end{bmatrix} \begin{matrix} 4 \\ 1 \\ 2 \\ 4 \\ 5 \end{matrix} \rightarrow R_1 = K_1 q_1 - Q_1 = K_1 T_1 q_1^* - Q_1 = \begin{bmatrix} 64.859 \\ 58.212 \\ -55.141 \end{bmatrix}$$

= 2.074074

ks = -400

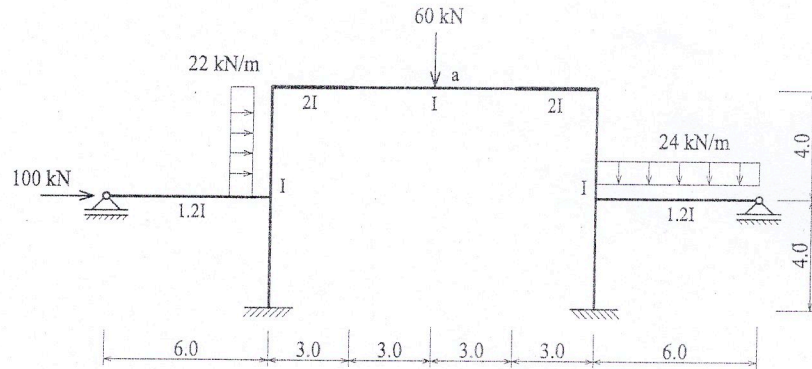


71 ] 4  
071 ] 1  
29 ] 2  
4  
5

5. Za dati nosač:

- a) Za simetričan slučaj opterećenja nacrtati dijagram momenata
- b) Odrediti vertikalno pomeranje tačke a

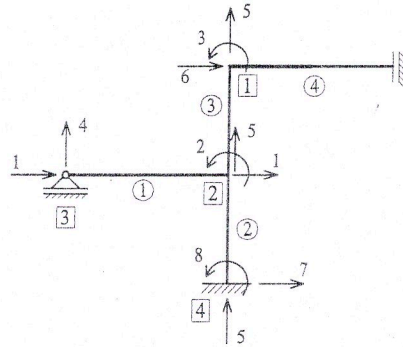
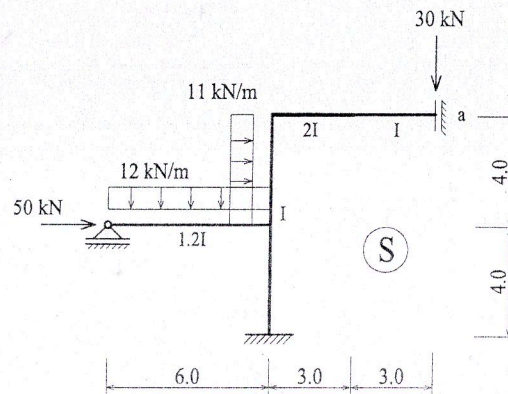
**Napomena:** Uticaj normalnih sila na deformaciju zanemariti.



2.725 ]  
-58.202 ]  
7.275 ]

Rešenje:

a) Simetrija:



Nepoznata pomeranja su  $q_1^*$ ,  $q_2^*$ ,  $q_3^*$ ,

Matrice krutosti štapova

-štap 1:

$$\mathbf{K}_1^* = \mathbf{K}_1 = EI \begin{bmatrix} 0.0167 & -0.0167 & 0.100 \\ -0.0167 & 0.0167 & -0.100 \\ 0.100 & -0.100 & 0.600 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 2 \end{matrix}$$

-štap 2:

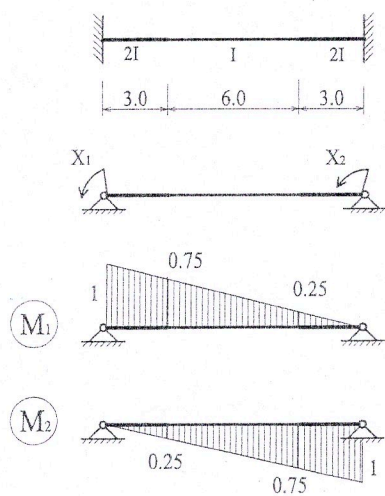
$$\mathbf{K}_2^* = \mathbf{K}_2 = EI \begin{bmatrix} 0.1875 & 0.375 & -0.1875 & 0.375 \\ 0.375 & 1.0 & -0.375 & 0.5 \\ -0.1875 & -0.375 & 0.1875 & -0.375 \\ 0.375 & 0.5 & -0.375 & 1.0 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 7 \\ 8 \end{matrix}$$

-štap 3:

$$K_3^* = K_3 = EI \begin{bmatrix} 6 & 3 & 1 & 2 \\ 0.1875 & 0.375 & -0.1875 & 0.375 \\ 0.375 & 1.0 & -0.375 & 0.5 \\ -0.1875 & -0.375 & 0.1875 & -0.375 \\ 0.375 & 0.5 & -0.375 & 1.0 \end{bmatrix} \begin{matrix} 6 \\ 3 \\ 1 \\ 2 \end{matrix}$$

-štap 4:

Štap 4 je štap tipa "s". Štap tipa "s" nastaje kada osa simetrije polovi horizontalni štap tipa "k" isključivo u simetriji. Kako je štap 4 i promenljivog poprečnog preseka, matrica krutosti mora se izvesti iz izvornog štapa tipa "k":



$$I_c = I$$

$$EI_c \alpha_{ii'} = \frac{I_c}{I} \int_s M_1^2 ds = 2.8125$$

$$EI_c \beta_{ii'} = \frac{I_c}{I} \int_s M_1 M_2 ds = -1.6875$$

$$\Delta = \alpha_{ii'}^2 - \beta_{ii'}^2 = 2.1826^2 - 1.6875^2 = 5.0625$$

$$a_{ii'} = \frac{\alpha_{ii'}}{\Delta} = 0.5556$$

$$b_{ii'} = -\frac{\beta_{ii'}}{\Delta} = 0.3333$$

$$e_{is} = \alpha_{ii'} - b_{ii'} = 0.2222$$

$$K_4 = K_4^* = EI \begin{bmatrix} 5 & 3 \\ 0 & 0 \\ 0 & 0.2222 \end{bmatrix} \begin{matrix} 5 \\ 3 \end{matrix}$$

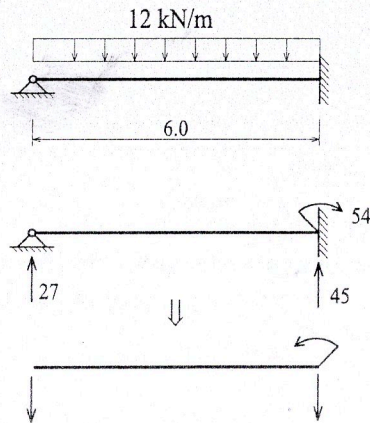
-submatrica krutosti nepoznatih:

$$K_{nn}^* = EI \begin{bmatrix} 1 & 2 & 3 \\ 0.375 & 0 & -0.375 \\ 0 & 2.60 & 0.50 \\ -0.375 & 0.50 & 1.2222 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}$$



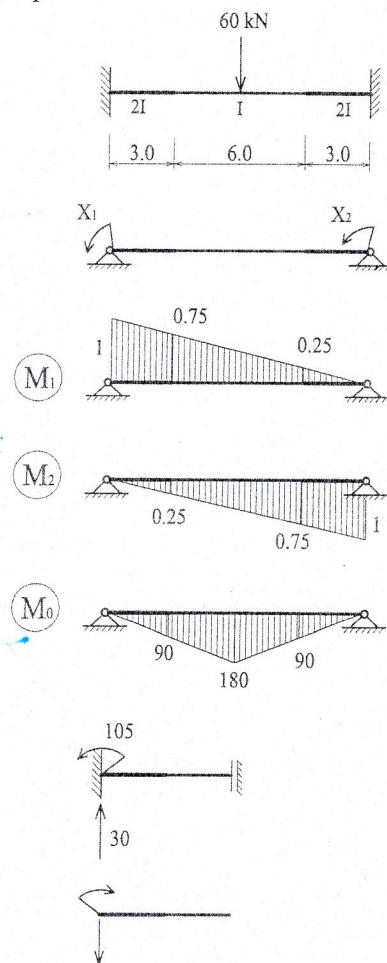
## Vektor ekvivalentnog opterećenja

-štap 1:



$$\mathbf{Q}_1^* = \begin{bmatrix} -27 \\ -45 \\ 54 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 2 \end{matrix}$$

-štap 4:



$$EI\delta_{11} = \frac{I_c}{I} \int_s M_1^2 ds = 2.8125$$

$$EI\delta_{12} = \frac{I_c}{I} \int_s M_1 M_2 ds = -1.6875$$

$$EI\delta_{22} = \frac{I_c}{I} \int_s M_2^2 ds = 2.8125$$

$$EI_c\delta_{10} = \frac{I_c}{I} \int_s M_1 M_0 ds = -472.50$$

$$EI_c\delta_{20} = \frac{I_c}{I} \int_s M_2 M_0 ds = 472.5$$

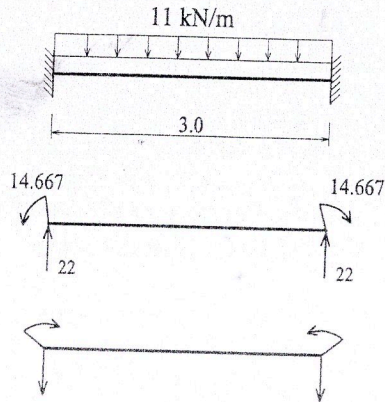
$$\mathbf{DX} + \delta = 0$$

$$\begin{bmatrix} \delta_{11} & \delta_{12} \\ \delta_{21} & \delta_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \delta_{10} \\ \delta_{20} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$x_1 = 105 \quad x_2 = -105$$

$$\mathbf{Q}_4 = \mathbf{Q}_4^* = \begin{bmatrix} -30 \\ -105 \end{bmatrix} \begin{matrix} 5 \\ 3 \end{matrix}$$

-štap 3:



$$Q_3^* = \begin{bmatrix} -22 \\ 14.667 \\ -22 \\ -14.667 \end{bmatrix} \begin{matrix} 6 \\ 3 \\ 1 \\ 2 \end{matrix}$$

Vektor slobodnih članova

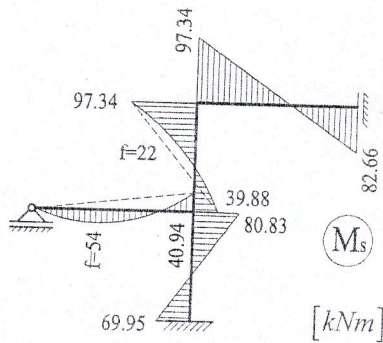
$$Q_n^* = \begin{bmatrix} 22.0 \\ 39.333 \\ -90.333 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix} \quad P_n^* = \begin{bmatrix} 50 \\ 0 \\ 0 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix} \quad \rightarrow \quad S_n^* = Q_n^* + P_n^* = \begin{bmatrix} 72.0 \\ 39.333 \\ -90.333 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}$$

-uslovne jednačine i rešenje:

$$K_{nn}^* q_n^* = S_{nn}^* \quad \rightarrow \quad q_n^* = \frac{1}{EI} \begin{bmatrix} 157.519 \\ 21.759 \\ -34.481 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}$$

Sile na krajevima štapa:

$$R_i = K_i q_i - Q_i \quad \rightarrow \quad M_s$$



4  
5  
2

2.8125

s = -1.6875

2.8125

s = -472.50

s = 472.5

$$\begin{bmatrix} \\ \\ \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

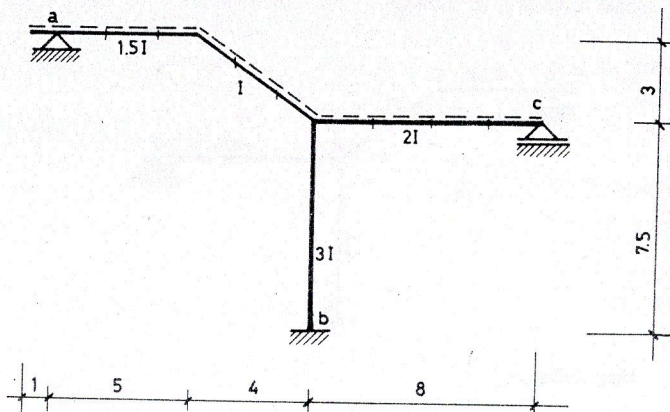
-105

MAJ 1985.

ZADACI

1.

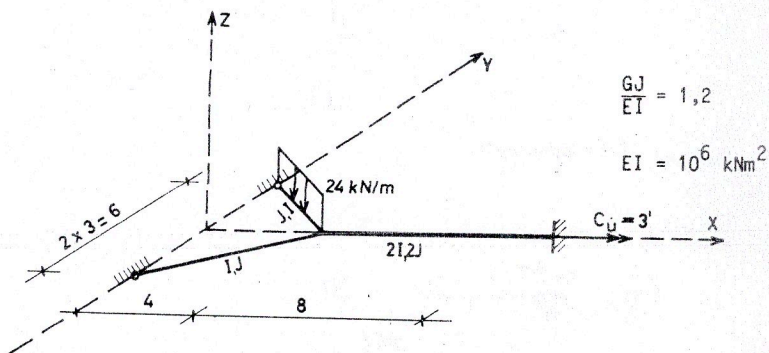
Za dati nosač, primenom približne metode deformacije, nacrtati uticajnu liniju za vertikalnu reakciju oslonca  $a$ , sa ordinatama u označenim tačkama.



2.

Za dati roštilj formirati matricu krutosti sistema i vektor ekvivalentnog opterećenja. Sračunati pomeranja čvorova i sile u štapovima usled:

- a) opterećenja
- b) obrtanja uklještenja  $c_u = 3$



$$\frac{GJ}{EI} = 1,2$$

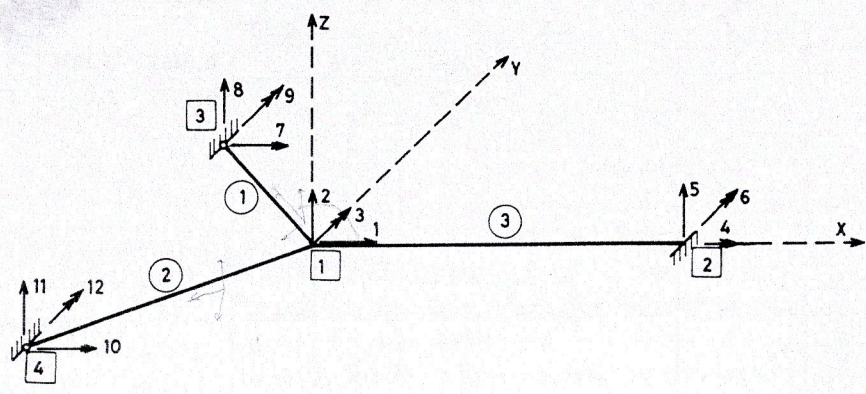
$$EI = 10^6 \text{ kNm}^2$$

3)

i)  $-4 \cdot 1,25 \xi'$

a
1739
000
7839
5757
3831
2140
1087
0393
0036
0154
0176
0110

2. Šema nosača



Nepoznata pomeranja: 1,2,3

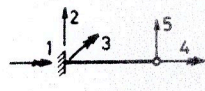
	i	k	cos	sin	J	I	l
1	1	3	-0,8	0,6	J	I	5
2	1	4	-0,8	-0,6	J	I	5
3	1	2	1	0	2J	2I	8

$\frac{GJ}{EI} = 1,2$

Matrice krutosti štapova

$$K_g = EI \begin{bmatrix} GJ/EI \cdot 1 & & & & GJ/EI \cdot 1 \\ & 3/l^3 & -3/l^2 & & -3/l^2 \\ & -3/l^2 & 3/l & & 3/l^2 \\ -GJ/EI \cdot 1 & & & & GJ/EI \cdot 1 \\ & -3/l^3 & 3/l^2 & & 3/l^3 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{matrix}$$

$$K_1 = K_2 = EI \begin{bmatrix} 0,24 & & & & -0,24 \\ & 0,024 & -0,12 & & -0,024 \\ & -0,12 & 0,6 & & 0,12 \\ -0,24 & & & & 0,24 \\ & -0,024 & 0,12 & & 0,024 \end{bmatrix}$$



$$K_3 = K_3^* = EI \begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 \\ 0,30 & & & -0,30 & & \\ & 0,0469 & -0,1875 & & -0,0469 & -0,1875 \\ & -0,1875 & 1,0 & & 0,1875 & 0,5 \\ -0,30 & & & 0,30 & & \\ & -0,0469 & 0,1875 & & 0,0469 & 0,1875 \\ & -0,1875 & 0,5 & & 0,1875 & 1,0 \\ & & & & & & 1 \\ & & & & & & 2 \\ & & & & & & 3 \\ & & & & & & 4 \\ & & & & & & 5 \\ & & & & & & 6 \end{bmatrix}$$

 $K_1^* =$  $K_1^* =$ 

Matrice transformacije

$$T_1 = \begin{bmatrix} -0,8 & 0 & 0,6 \\ 0 & 1 & 0 \\ -0,6 & 0 & -0,8 \\ & -0,8 & 0 & 0,6 \\ & 0 & 1 & 0 \end{bmatrix}$$

 $K_2^* =$ 

$$T_2 = \begin{bmatrix} -0,8 & 0 & -0,6 \\ 0 & 1 & 0 \\ 0,6 & 0 & -0,8 \\ & -0,8 & 0 & -0,6 \\ & 0 & 1 & 0 \end{bmatrix}$$

Matr

$$\hat{K}_i = K_i T_i$$

$$\hat{K}_1 = EI \begin{bmatrix} 1 & 2 & 3 & 7 & 8 & 9 \\ -0,192 & 0 & 0,144 & 0,192 & 0 & -0,144 \\ 0,072 & 0,024 & 0,096 & 0 & -0,024 & 0 \\ -0,36 & -0,12 & -0,48 & 0 & 0,12 & 0 \\ 0,192 & 0 & -0,144 & -0,192 & 0 & 0,144 \\ -0,072 & -0,024 & -0,096 & 0 & 0,024 & 0 \end{bmatrix}$$

$$\hat{K}_2 = EI \begin{bmatrix} 1 & 2 & 3 & 10 & 11 & 12 \\ -0,192 & 0 & -0,144 & 0,192 & 0 & 0,144 \\ -0,072 & 0,024 & 0,096 & 0 & -0,024 & 0 \\ 0,36 & -0,12 & -0,48 & 0 & 0,12 & 0 \\ 0,192 & 0 & 0,144 & -0,192 & 0 & -0,144 \\ 0,072 & -0,024 & -0,096 & 0 & 0,024 & 0 \end{bmatrix}$$

$$K^* = EI \begin{bmatrix} 1 & 2 \\ 1,0392 & 0 \\ 0 & 0,094 \\ 0 & 0,004 \\ -0,3 & \\ & -0,046 \\ & -0,187 \\ -0,1536 & \\ -0,072 & -0,024 \\ 0,1152 & \\ -0,1536 & \\ 0,072 & -0,024 \\ -0,1152 & \end{bmatrix}$$

	6	
469	-0,1875	1
875	0,5	2
		3
		4
469	0,1875	5
875	1,0	6

$$K_i^* = T_i^T \hat{K}_i$$

$$K_1^* = EI$$

	1	2	3	7	8	9	
0,3696	0,072	0,1728	-0,1536	-0,072	0,1152		1
0,072	0,024	0,096	0	-0,024	0		2
0,1728	0,096	0,4704	0,1152	-0,096	-0,0864		3
-0,1536	0	0,1152	0,1536	0	-0,1152		7
-0,072	-0,024	-0,096	0	0,024	0		8
0,1152	0,0	-0,0864	-0,1152	0	0,0864		9

$$K_2^* = EI$$

	1	2	3	10	11	12	
0,3696	-0,072	-0,1728	-0,1536	0,072	-0,1152		1
-0,072	0,024	0,096	0	-0,024	0		2
-0,1728	0,096	0,4704	-0,1152	-0,096	-0,0864		3
-0,1536	0	-0,1152	0,1536	0	0,1152		10
0,072	-0,024	-0,096	0	0,024	0		11
-0,1152	0	-0,0864	0,1152	0	0,0864		12

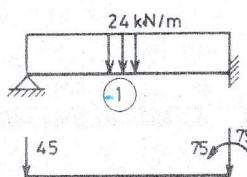
Matrica krutosti sistema

	1	2	3	4	5	6	7	8	9	10	11	12	
1,0392	0	0	-0,3				-0,1536	-0,072	0,1152	-0,1536	0,072	-0,1152	1
0	0,0949	0,0045		-0,0469	-0,1875			-0,024			-0,024		2
0	0,0045	1,9408		-0,1875	0,5		0,1152	-0,096	-0,0864	-0,1152	-0,096	-0,0864	3
-0,3			0,3										4
		-0,0469	0,1875		0,0469	0,1875							5
		-0,1875	0,5		0,1875	1,0							6
-0,1536			0,1152				0,1536		-0,1152				7
-0,072	-0,024	-0,096						0,024					8
0,1152		-0,0864					-0,1152		0,0864				9
-0,1536		-0,1152								0,1536		0,1152	10
0,072	-0,024	-0,096									0,024		11
-0,1152		-0,0864								0,1152		0,0864	12

9	
-0,144	
0	
0	
0,144	
0	
12	
0,144	
0	
0	
-0,144	
0	

a) Opterećenje

Vektor ekvivalentnog opterećenja



$$Q_1 = \begin{bmatrix} 0 \\ -75 \\ 75 \\ 0 \\ -45 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 7 \\ 8 \end{matrix} \quad Q_1^* = T_1^T Q_1 = \begin{bmatrix} -45 \\ -75 \\ -60 \\ 0 \\ -45 \\ 0 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 7 \\ 8 \\ 9 \end{matrix} = \begin{bmatrix} Q_n^* \\ Q_p^* \end{bmatrix}$$

Uslovne jednačine i rešenje

$$K_{nn}^* q_n^* = Q_n^* \quad q_n^* = \frac{1}{EI} \begin{bmatrix} -43,3025 \\ -788,9264 \\ -29,0859 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}$$

Vektori sila na krajevima štapova

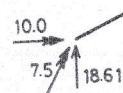
$$R_i = \hat{K}_i q_i^* - Q_i$$

$$R_1 = \begin{bmatrix} 4,126 \\ -24,844 \\ 124,221 \\ -4,126 \\ 24,844 \end{bmatrix} - \begin{bmatrix} 0 \\ -75 \\ 75 \\ 0 \\ -45 \end{bmatrix} = \begin{bmatrix} 4,126 \\ 50,156 \\ 49,221 \\ -4,126 \\ 69,844 \end{bmatrix}$$

$$R_2 = \begin{bmatrix} 12,503 \\ -18,609 \\ 93,044 \\ -12,503 \\ 18,609 \end{bmatrix} \quad R_3 = \begin{bmatrix} -12,991 \\ -31,547 \\ 118,838 \\ 12,991 \\ 31,547 \\ 133,381 \end{bmatrix}$$

Vektor reakcija oslonaca

$$S_p^* = K_{pn}^* q_n^* - Q_p^* = \begin{bmatrix} 12,991 \\ 31,547 \\ 133,381 \\ 3,301 \\ 24,844 \\ -2,475 \\ 10,002 \\ 18,609 \\ 7,502 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -45 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 12,991 \\ 31,547 \\ 133,381 \\ 3,301 \\ 69,844 \\ -2,475 \\ 10,002 \\ 18,609 \\ 7,502 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \end{matrix}$$



b) Of

 $q_4^* =$  $K_{nn}$  $K_{nn}$ 

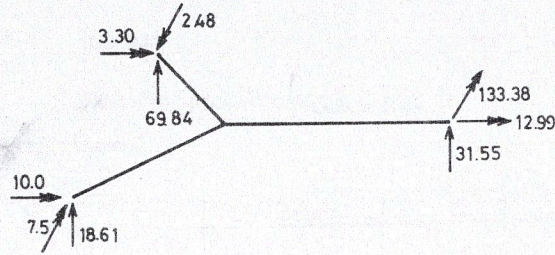
Uslo

 $q_n^*$ 

Vek

 $R_1$  $R_3$

$$T_1^T Q_1 = \begin{bmatrix} -45 & 1 \\ -75 & 2 \\ -60 & 3 \\ 0 & 7 \\ -45 & 8 \\ 0 & 9 \end{bmatrix} = \begin{bmatrix} Q_n^* \\ Q_p^* \end{bmatrix}$$



$$\Sigma Z = 0$$

$$\Sigma M_t = 0$$

$$\Sigma M_y = 0$$

b) Obrtanje uklještenja

$$q_4^* = 3' = 0,0008726 \text{ rad}$$

$$K_{nn} q_n^* + K_{np} q_p^* = 0$$

$$K_{nn} q_n^* = -K_{np} q_4^*$$

Uslovne jednačine i rešenja

$$\begin{bmatrix} 1,0392 & & \\ & 0,0949 & 0,0045 \\ & 0,0045 & 1,9408 \end{bmatrix} \begin{bmatrix} q_1^* \\ q_2^* \\ q_3^* \end{bmatrix} = \begin{bmatrix} 2,618 \\ 0 \\ 0 \end{bmatrix} \cdot 10^{-4} EI$$

$$q_n^* = 10^{-4} \begin{bmatrix} 2,5192 \\ 0 \\ 0 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \end{matrix}$$

Vektori sila na krajevima štapova:  $R_i = \hat{K}_i q_i^*$

$$R_1 = \begin{bmatrix} -48,4 \\ 18,1 \\ -90,7 \\ 48,4 \\ -18,1 \end{bmatrix} \quad R_2 = \begin{bmatrix} -48,4 \\ -18,1 \\ 90,7 \\ 48,4 \\ 18,1 \end{bmatrix}$$

$$R_3 = \begin{bmatrix} -186,2 \\ 0 \\ 0 \\ 186,2 \\ 0 \\ 0 \end{bmatrix}$$



$\kappa_1 = \frac{EJ}{l^3}$

6	1	2	3	6
12	6l	-12	6l	6
	4l <sup>2</sup>	-6l	2l <sup>2</sup>	1
		12	-6l	2
			4l <sup>2</sup>	3

$\kappa_2 = \frac{EJ}{l^3}$

2	3	7	4	2
12	6l	-12	6l	2
	4l <sup>2</sup>	-6l	2l <sup>2</sup>	3
		12	-6l	7
			4l <sup>2</sup>	4

$\kappa_{SS}^*$

1	2	3	4	1
$\frac{4EJ}{l} + C_{p1}$	$-\frac{6EJ}{l^2}$	$\frac{2EJ}{l}$	0	1
	$\frac{2EJ}{l^2} + C_y$	0	$\frac{6EJ}{l^2}$	2
		$\frac{EJ}{l}$	$\frac{2EJ}{l}$	3
			$\frac{4EJ}{l} + C_{p2}$	4

$Q_1 = \begin{bmatrix} -\frac{qL}{2} \\ -\frac{qL^2}{12} \\ -\frac{qL}{2} \\ \frac{qL^2}{12} \end{bmatrix}$

$Q_2 = \begin{bmatrix} -\frac{qL}{2} \\ -\frac{qL^2}{12} \\ -\frac{qL}{2} \\ \frac{qL^2}{12} \end{bmatrix}$

$Q_S^* = \begin{bmatrix} -\frac{qL^2}{12} \\ -qL \\ 0 \\ \frac{qL^2}{12} \end{bmatrix}$

$Q_{SS}^* = \begin{bmatrix} \\ \\ \\ \end{bmatrix}$

$EJ = 20.000 \text{ kNm}^2; \quad q = 20 \text{ kN/m}; \quad l = 4 \text{ m}$

1°  $C_{p1} = C_{p2} = \infty; \quad C_y = 0$

$q = \begin{bmatrix} 0 & -0,010667 & 0 & 0 \end{bmatrix}$

$R_1 = \begin{bmatrix} 80 & 106,67 & 0 & 53,33 \end{bmatrix}$

$R_2 = \begin{bmatrix} 0 & -53,33 & 80 & -106,67 \end{bmatrix}$

2°  $C_{p1} = C_{p2} = 0; \quad C_y = \infty$

$q = \begin{bmatrix} -0,001333 & 0 & 0 & 0,001333 \end{bmatrix}$

$R_1 = \begin{bmatrix} 30 & 0 & 50 & -40 \end{bmatrix}$

$R_2 = \begin{bmatrix} 50 & 40 & 30 & 0 \end{bmatrix}$

3°  $C_{p1} = 0; \quad C_{p2} = \infty; \quad C_y = 0$

$q = \begin{bmatrix} -0,010667 & -0,021333 & 0,002667 & 0 \end{bmatrix}$

$R_1 = \begin{bmatrix} 60 & 0 & 20 & 80 \end{bmatrix}$

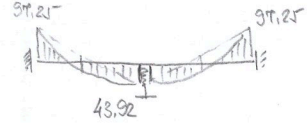
$R_2 = \begin{bmatrix} -20 & -80 & 100 & -160 \end{bmatrix}$

4°  $C_{p1} = C_{p2} = \infty$   
 $C_y = 1000$

$q = \begin{bmatrix} 1 & 2 & 3 & 4 \\ 0 & -0,0094117 & 0 & 0 \end{bmatrix}$

$R_1 = \begin{bmatrix} 6 & 1 & 2 & 3 \\ 75,29 & 97,25 & 47,71 & 43,92 \end{bmatrix}$

$R_2 = \begin{bmatrix} 2 & 3 & 7 & 4 \\ 4,771 & -43,92 & 15,29 & -97,25 \end{bmatrix}$

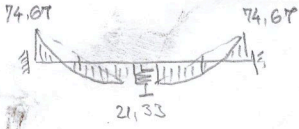


5°  $C_{p1} = C_{p2} = \infty$   
 $C_y = 5000$

$q = \begin{bmatrix} 0 & -0,0064 & 0 & 0 \end{bmatrix}$

$R_1 = \begin{bmatrix} 6 & 1 & 2 & 3 \\ 64 & 74,67 & 16 & 21,33 \end{bmatrix}$

$R_2 = \begin{bmatrix} 2 & 3 & 7 & 4 \\ 16 & -21,33 & 64 & -74,67 \end{bmatrix}$



6°  $C_{p1} = C_{p2} = \infty$   
 $C_y = 50.000$

$q = \begin{bmatrix} 0 & -0,00391 & 0 & 0 \end{bmatrix}$

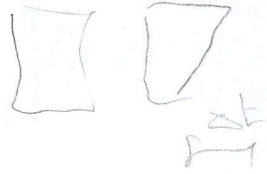
$R_1 = \begin{bmatrix} 6 & 1 & 2 & 3 \\ 45,22 & 37,10 & 34,78 & -16,23 \end{bmatrix}$

$R_2 = \begin{bmatrix} 2 & 3 & 7 & 4 \\ 34,78 & 16,23 & 45,22 & -37,10 \end{bmatrix}$



7°  $C_{p1} = C_{p2} = \infty$   
 $C_y = \infty$   
 $q = 0$

Site na kragenima stepova su jeduak ekv. opt.



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